

- A. Graph P_1/P_1° vs. ϕ_1 for $\chi_1 = 0, 0.25, 0.50, 0.75$ and 1.0 at $N=100$ and at $N=1000$. Overlay on each of the two graphs that of ideal solution prediction, given by (2)

$$P_1/P_1^\circ = \phi_1 \cdot \exp \left[\left(1 - \frac{1}{N}\right)(1 - \phi_1) + \chi_1(1 - \phi_1)^2 \right] \quad (1)$$

$$P_1/P_1^\circ = X_1 = \frac{N\phi_1}{N\phi_1 + (1 - \phi_1)} \quad (2)$$

- B. Plot $-\frac{\mu_1 - \mu_1^\circ}{RT}$ vs. ϕ_2 for a range of $0 \leq \phi_2 \leq 0.05$ for $\chi_1 = 0, 0.50, 0.532, 0.54, 0.55$ and 0.56 at $N=1000$. Find the inflection point by setting

$$\left(\frac{\partial \mu_1}{\partial \phi_1} \right)_{T,P} = 0, \text{ and } \left(\frac{\partial^2 \mu_1}{\partial \phi_1^2} \right)_{T,P} = 0$$

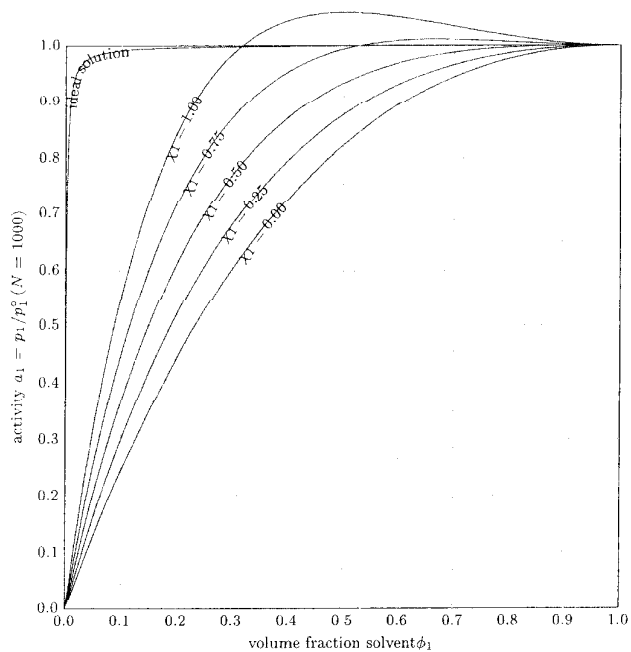
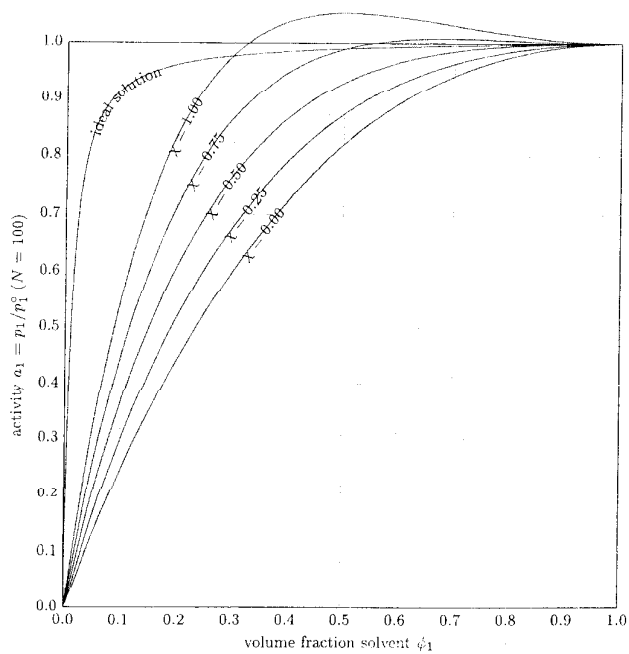
and determine $\chi_{1,C}$ and $\phi_{2,C}$ at the inflection point.

$$-\frac{\mu_1 - \mu_1^\circ}{RT} = -\left[\ln(1 - \phi_2) + \left(1 - \frac{1}{N}\right)\phi_2 + \chi_1\phi_2^2 \right] \quad (3)$$

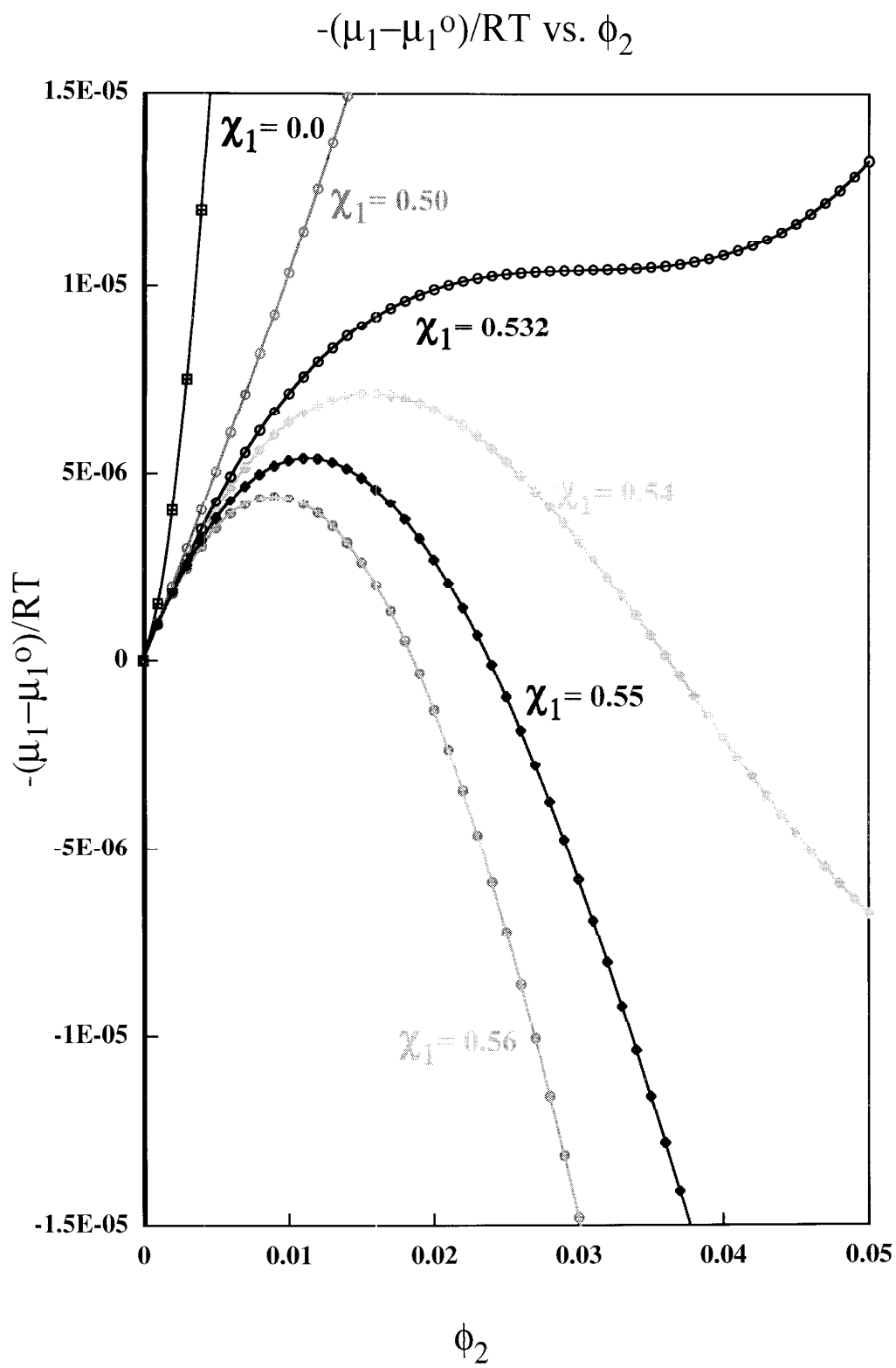
- C. 3.15
D. 3.18
E. 3.21
F. 3.24
G. 3.25
H. 3.26
I. 3.27

A.

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B.



$$\phi_{2,c} = \frac{1}{1 + N^{1/2}} \approx 0.031$$

$$\chi_{1,c} = \frac{(1 + N^{1/2})^2}{2N} = 0.532$$

C. (3.15)

Helmholtz Free Energy and force for stretching a chain with an arbitrary scaling exponent ν with $R_0 = bN^\nu$. Follow the procedure similar to those for $R_F = bN^{3/5}$.

$$\xi \approx b g^\nu, \quad R_f \approx \xi \frac{N}{g} \approx \xi \frac{N}{(\xi/b)^{1/\nu}} \approx bN \left(\frac{b}{\xi} \right)^{(1-\nu)/\nu}$$

$$\therefore \xi \approx \frac{(bN)^{\frac{\nu}{1-\nu}} \cdot b}{R_f^{\frac{\nu}{1-\nu}}} \approx b \left(\frac{bN}{R_f} \right)^{\frac{\nu}{1-\nu}}$$

$$A(N, R_f) \approx kT \frac{N}{g} \approx kTN \left(\frac{b}{\xi} \right)^{1/\nu} \approx kTN \left(\frac{R_f}{bN} \right)^{\frac{\nu}{1-\nu}}$$

$$f \approx \frac{kT}{\xi} \approx \frac{kT}{b} \left(\frac{R_f}{bN} \right)^{\frac{\nu}{1-\nu}} \approx \frac{kT}{R_0} \left(\frac{R_f}{R_0} \right)^{\frac{\nu}{1-\nu}}$$

$$\begin{aligned} b(bN)^{\frac{\nu}{1-\nu}} &= bN^\nu N^{-\nu} (bN)^{\frac{\nu}{1-\nu}} \\ &= bN^\nu [N^{-\nu(1-\nu)} bN]^{\frac{\nu}{1-\nu}} \\ &= bN^\nu [N^{-1+\nu} bN]^{\frac{\nu}{1-\nu}} \\ &= R_0 \cdot R_0^{\frac{\nu}{1-\nu}} \end{aligned}$$

D. (3.18) D , thickness of an adsorbed chain with $R_0 = bN^\nu$ with the interaction energy per monomer in contact with the surface ϵ .

$$A_{\text{int}} \approx -\epsilon kTN \frac{b}{D}, \quad A_{\text{confinement}} \approx kTN \left(\frac{b}{D} \right)^{1/\nu} \quad (\text{Eq. 3.49})$$

$$A_{\text{total}} \approx -\epsilon kTN \left(\frac{b}{D} \right) + kTN \left(\frac{b}{D} \right)^{1/\nu}, \quad \left(\frac{\partial A_{\text{total}}}{\partial D} \right)_T = 0$$

$$+\varepsilon kTN \frac{b}{D^2} - \frac{1}{\nu} kTN \frac{b^{1/\nu}}{D^{1+1/\nu}} = 0$$

$$\varepsilon \frac{b}{D^2} = \frac{1}{\nu} \frac{b^{1/\nu}}{D^{1+1/\nu}}, \quad \frac{D^2}{D \cdot D^{1/\nu}} \approx \frac{\varepsilon \nu b}{b^{1/\nu}}$$

$$D^{1-1/\nu} \approx \varepsilon \nu b^{1-1/\nu}, \quad D \approx (\varepsilon \nu)^{\frac{\nu}{\nu-1}} \cdot b$$

$$\approx \frac{b}{(\nu \varepsilon)^{\nu/(1-\nu)}} \approx \frac{b}{\varepsilon^{\nu/(1-\nu)}}$$

$$A_{\text{confinement}} \approx kTN \left(\frac{b}{D} \right)^{1/\nu} \approx kTN (\nu \varepsilon)^{\frac{1}{1-\nu}} \approx kTN \varepsilon^{\frac{\nu}{1-\nu}}$$

$\uparrow$
 $\frac{b}{D} \approx (\nu \varepsilon)^{\frac{\nu}{1-\nu}}$

E.(3.2i) Polymer adsorption from good solvent
 $-\varepsilon kT$ attractive energy

(i) $D \approx b/\varepsilon^{3/2}$ (eq. 3.59)

(ii) $N=10^3$, $b=3\text{\AA}$, $\varepsilon=0.4$

$$\xi_{\text{ads}} \approx D \approx \frac{b}{\varepsilon^{3/2}} \approx 12\text{\AA}$$

(iii) Minimal force to pull away at a.t.

$$f \approx \frac{kT}{\xi_{\text{ads}}} \approx \frac{1.38 \cdot 10^{-23} \cdot 300}{1.2 \cdot 10^{-9}} \approx 3.45 \cdot 10^{-12} \text{ N}$$

$= 3.45 \text{ pN}$

(iv) $2f = 6.9 \text{ pN}$, pull out 2 lobes at a time

(v) $D \approx b/\varepsilon \approx \xi_{\text{ads}}$, $f \approx \frac{kT}{(b/\varepsilon)} \approx \frac{1.38 \cdot 10^{-23} \cdot 300 \cdot 0.4}{0.3 \cdot 10^{-9}} \approx 5.52 \text{ pN}$
 Adsorption is stronger.

F. (3.24)

$$R_F \rightarrow 4R_F = R_f$$

$$f \approx \frac{kT}{R_F} \left(\frac{R_f}{R_F} \right)^{3/2} \quad (\text{Eq. 3.38}), \quad R_F \approx v^{1/5} b^{2/5} N^{3/5} \approx 20 \cdot 10^{-9} \text{ m}$$

$$kT \approx 4.14 \cdot 10^{-21} \text{ J/molecule}$$

$$f \approx \frac{kT}{R_F} \left(\frac{4R_F}{R_F} \right)^{3/2} \approx \frac{8kT}{R_F} \approx 1.65 \text{ pN}$$

which is valid because $\xi_{\text{extension}} \approx 6.3b > \xi_T \approx 3.3b$

G. (3.25)

$$(i) \quad \xi_T \approx b^4/v, \quad g_T \approx b^6/v^2$$

(ii) Size of compression blob $\approx$ slit dimension D

$$(iii) \quad D \approx v^{1/5} b^{2/5} g^{3/5} \text{ for } D > \xi_T \approx b^4/v$$

$$\text{Thus, } g_{\text{com}} \approx D^{5/3} / v^{1/3} b^{2/3} \text{ if } D > \xi_T$$

$$g'_{\text{com}} \approx (D/b)^2 \text{ if } D < \xi_T \approx b^4/v$$

(iv) With $D > \xi_T \approx b^4/v$

$$A_{\text{confinement}} \approx kT \frac{N}{g_{\text{com}}} \approx kTN \frac{v^{1/3} b^{2/3}}{D^{5/3}} \approx kT \left(\frac{v^{1/5} b^{2/5} N^{3/5}}{D} \right)^{5/3}$$

$$\approx kT \left(\frac{R_F}{D} \right)^{5/3}$$

With $D < \xi_T$

$$A_{\text{confinement}} \approx kT \frac{N}{g'_{\text{com}}} \approx kTN \left(\frac{b}{D} \right)^2 \approx kT \left(\frac{R_0}{D} \right)^2$$

(v) The crossover from $D > \xi_T$ to $D < \xi_T$ should be at $D \approx \xi_T \approx b^4/v \approx \frac{(5\text{\AA})^4}{20\text{\AA}^3} \approx \frac{25 \cdot 25}{20} \text{\AA} \approx 31\text{\AA}$

H(3.26)

For randomly branched polymer in solution

$$(i) A \approx kT \left(\frac{3}{2} \frac{R^2}{R_0^2} + v \frac{N^2}{R^3} \right) \quad (\text{Eq. 3.19})$$

where $R_0 = bN^{1/4}$ for this polymer

$$\left(\frac{\partial A}{\partial R} \right)_T = kT \left[\frac{3}{2} \cdot 2(R/R^2) - 3vN^2/R^4 \right] = 0$$

$$\frac{3R}{R_0^2} \approx vN^2/R^4, \quad R^5 \approx vN^2 b^2 N^{1/2} \approx v b^2 N^{5/2}$$

$$\boxed{R \approx v^{1/5} b^{2/5} N^{1/2}}$$

(ii) $\xi_T \approx b g_T^{1/4}$, g_T can be estimated from

$$kT v \frac{g_T^2}{\xi_T^3} \approx kT, \quad g_T^2 \approx \frac{\xi_T^3}{v} \approx \frac{b^3 g_T^{3/4}}{v}$$

$$\underbrace{\hspace{1cm}}_{\text{analog of } \frac{vN^2}{R^3}}$$

$$g_T \approx \left(\frac{b^3}{v} \right)^{4/5} \approx \left(\frac{3^3 \text{\AA}^3}{2.7 \text{\AA}^3} \right)^{4/5}$$

$$\approx 6.3$$

Linear chain g_T

$$g_T \approx \left(\frac{b^3}{v} \right)^2$$

which is substantially different from $(b^3/v)^{4/5}$

(iii) $\xi_T \approx b g_T^{1/4} \approx b \cdot \left(\frac{b^3}{v} \right)^{1/5}$ Branched
 $\xi_T \approx b^4/v$ linear

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(iv)

$$R \approx b N^{1/4}$$

$$R \approx v^{1/5} b^{1/5} N^{1/2} \approx (2.7 \text{ \AA}^3)^{1/5} (3 \text{ \AA})^{1/5} (10^3)^{1/2} \\ \cong (1.22)(1.55)(31.6) \cong 60 \text{ \AA}$$

$$(v) R \approx (v b^2 N^3)^{1/5} \cong (2.7 \text{ \AA}^3 \cdot 3^2 \text{ \AA}^2 \cdot 10^9)^{1/5} \cong 119 \text{ \AA}$$

$$(vi) \xi_T \approx b \left(\frac{b^3}{v} \right)^{1/5} \cong 3 \left(\frac{3^3 \text{ \AA}^3}{2.7 \text{ \AA}^3} \right)^{1/5} \text{ \AA} \cong 3 \cdot 10^{1/5} \text{ \AA} \cong 4.8 \text{ \AA} \\ g_T \cong 6.3$$

$$(vii) \xi_T \approx b^4/v = \left(\frac{3^4 \text{ \AA}^4}{2.7 \text{ \AA}^3} \right) \cong 30 \text{ \AA}, \quad g_T \cong \left(\frac{b^3}{v} \right)^2 \cong 100$$

$$I(3.27) \quad v = \left(1 - \frac{\theta}{T} \right) b^3$$

$$N = 10^3, \quad b = 3 \text{ \AA}, \quad \theta = 303 \text{ K}$$

$$R_F \approx v^{1/5} b^{2/5} N^{3/5} \approx \left(1 - \frac{\theta}{T} \right)^{1/5} b^{3/5} \cdot b^{2/5} \cdot N^{3/5} \\ \approx \left(1 - \frac{\theta}{T} \right)^{1/5} b N^{3/5}$$

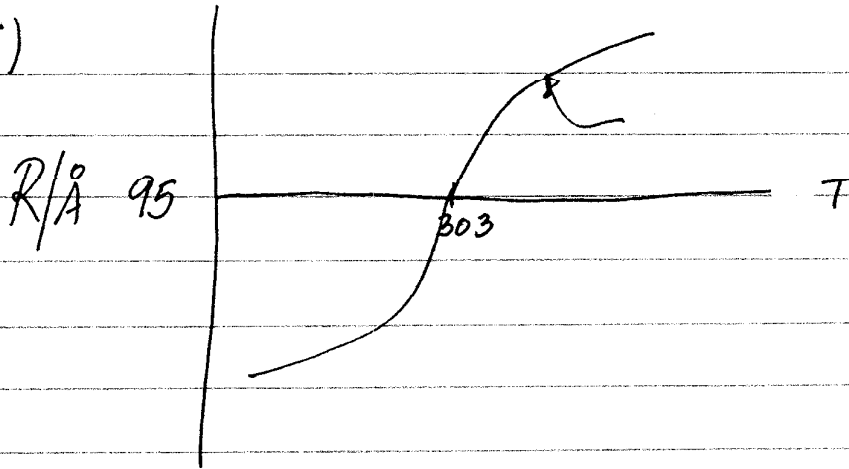
$$T = 60^\circ \text{C}, \quad R_F \approx \left(1 - \frac{303}{333} \right)^{1/5} (3 \text{ \AA}) (10^3)^{3/5} \\ \cong 117 \text{ \AA}$$

$$T = 30^\circ \text{C} \quad R \approx b N^{1/2} \cong 95 \text{ \AA}$$

$$T = 10^\circ \text{C (poor solvent)}$$

$$R_{gl} \approx b^2 \left(\frac{N}{v} \right)^{1/5} \approx b^2 \frac{10}{\left| \left(1 - \frac{\theta}{T} \right) b^3 \right|^{1/5}} \approx \frac{b \cdot 10}{\left(\frac{303}{283} - 1 \right)^{1/5}} \\ \cong \frac{30 \text{ \AA}}{0.41} \cong 73 \text{ \AA}$$

(ii)



$$(iii) \text{ At } 60^\circ\text{C} \quad g_T \approx \left(\frac{b^3}{v} \right)^2 \approx \left(1 - \frac{\theta}{T} \right)^{-2} \cong 123$$

$$(iv) \text{ At } 10^\circ\text{C} \quad g_T \approx \left(\frac{b^3}{101} \right)^2 \cong \left(\frac{\theta}{T} - 1 \right)^{-2} \cong 200$$